Task 55 Large Solar Heating & Cooling Systems

SOLAR HEATING & COOLING PROGRAMME
INTERNATIONAL ENERGY AGENCY

Seasonal pit heat storages - Guidelines for materials & construction

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Introduction

Seasonal pit heat storages in connection to large scale solar plants for district heating are now in use in several countries throughout the world. The concept can store seasonally, but has also the possibility for shorter heat storage periods, as it provides quick charging and discharging.

This fact sheet is a design guideline for pit heat storages – or "pit thermal energy storages" (PTES) – based on experience from the design and implementation of especially the Danish pit heat storages.

In principle a pit heat storage is a large water reservoir for storing of thermal energy. Water is an excellent medium for heat storing as it is cheap, non-toxic and has a high heat capacity. The cost of a water storage mainly consists of the parts surrounding the water: E.g. a watertight tank and thermal insulation. For smaller storages (up to 5 000 m^3) typically an insulated steel tank is used, but for larger storages a pit heat storage is considerably cheaper per m^3 water.

Design of the storage

The principal structure of a pit heat storage is quite simple, as it consists of an excavation in the ground covered with a watertight liner.

Figure 1. Picture of Dronninglund Pit Storage under construction. Dronninglund District heating; 37,573 m^2 of solar collectors and a 60,000 m^3 water in pit heat storage. (PlanEnergi)

The storage is filled with water and covered by a floating insulated cover. But to ensure a functioning and long-term durable storage the design must to be handled very carefully in every aspect. The main parts will be described in the following.

Shape and soil balance

The pit heat storage can be designed with different shapes but the simplest is an excavation shaped as a truncated pyramid placed upside down in the ground as shown in figure 2. To minimize the cost of soil handling and transportation the excavation is made with soil balance which means that the soil excavated from the bottom part of the storage is used as embankments around the upper part of the storage. The necessary volume of the storage depends on the overall system it is connected to and it is necessary to make a calculation model of the overall system to find the optimal volume.

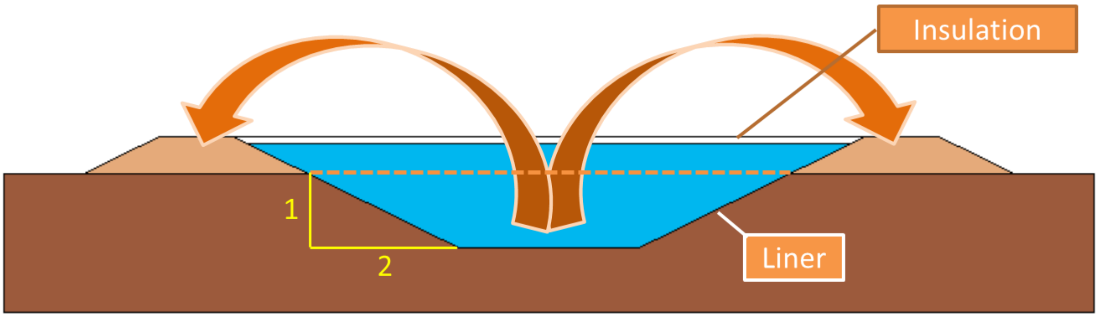

Figure 2. Principle sketch of a pit heat storage cross section.

Lining materials

Water tightness of a pit heat storage is obtained by covering the soil with a liner. Depending on the specific cover design a liner is also used for the insulated cover construction. The service life of a pit heat storage is very much dependent of the liner[1]. At the moment applicable liners for pit heat storages are considered different types of polymer liners (PP, PE), elastomer liners (EPDM) and different kinds of metal liners (stainless steel, aluminium). Until recently HDPE liners were often used for high temperatures (up to 90°C). Now a new PP liner seems to have a longer lifetime at high temperatures (up to 95°C). It is important to have a credible lifetime estimate from manufacturer for the specific estimated storage temperature time profile.

Polymer and elastomer liners are by far the cheapest regarding both material price and installation cost, but metal liners have an advantage regarding long term stability and vapour tightness.

Polymer liners

[1] Water sealing with special clay has been tested in earlier pit heat storages with poor results

Polymer liners as PP and PE are relatively cheap and easy to install with well documented welding and testing techniques. Therefore, they are widely used for geomembranes. The welding process is shown in figure 3.

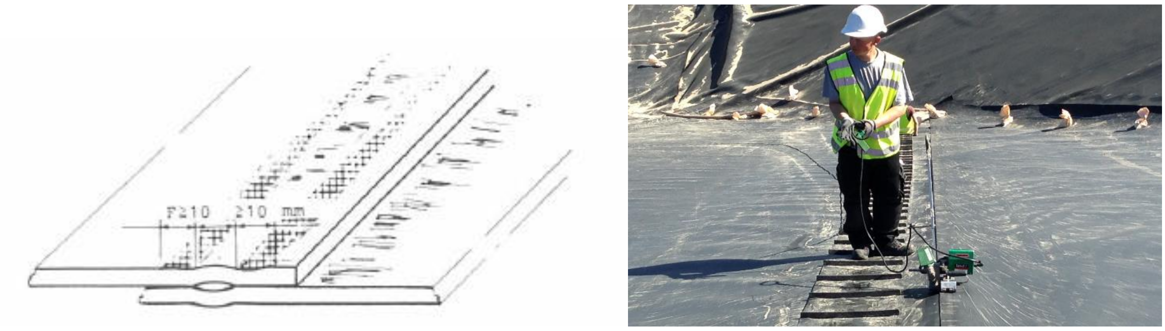

Figure 3. Double welding of a HDPE liner. The welding can be tested by applying pressurized air to the air channel between the welding seams.

The major issue regarding polymer liners is the temperature resistance and another disadvantage compared to metal liners is the water vapour permeability. For polymer liners the water vapour permeability is strongly temperature dependent (see figure 4). HDPE liners have the lowest water vapour permeability compared to other geomembranes. At 20°C the water vapour permeability is around 0.03 g/m^2/day for a 1 mm liner. For temperatures above 60°C it is difficult to get data from the suppliers, but experiments have shown a water vapour permeability for a 2.5 mm liner of app. 1.5 g/m^2/day at 80°C. [1]). For PP the water vapour permeability is more than 4 times as high as for HDPE. For comparison LDPE has a water vapour permeability 45 times as high and PVC 115 times as high as HDPE [3].

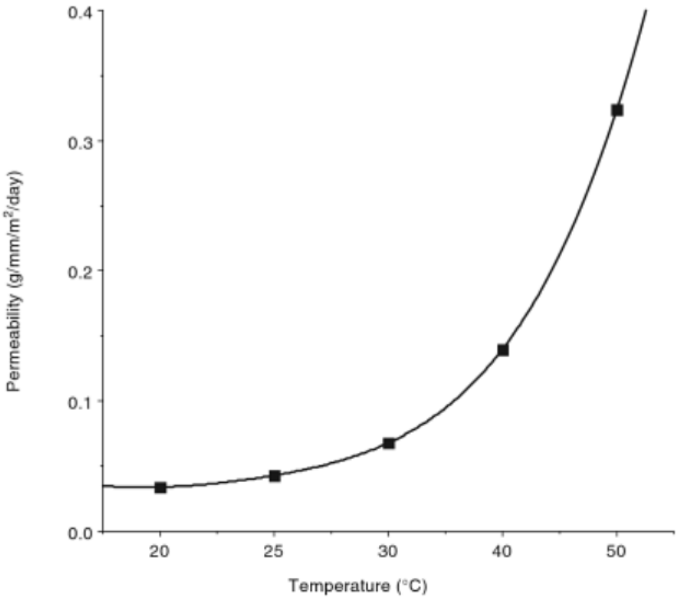

Figure 4. Water vapour permeability as a function of temperature for a typical HDPE liner [3]

The temperature resistance of a polymer liner is dependent on not only the base material but also highly on different additives to the material. But the additives will diffuse out of the material over time especially when exposed to hot water on one side and air/soil on the other side of the liner. A liner material with excellent temperature performance according to the supplier can therefore have very limited lifetime in a pit heat storage.

The Danish Technological Institute has developed a test method for an accelerated life test of polymer liners for pit heat storages. This can be used to test a sample of a liner but for the best liners the test should be expected to take more than a year. From the test results and the expected temperature profile of the storage through the year an expected service life of the liner can be predicted. The best liners tested by this method so far are specific high temperature developed HDPE liners which have an expected lifetime of not more than 3 years at a constant temperature of 90°C. For a typical temperature profile of a pit heat storage connected to a solar plant the lifetime of the liner can though be calculated to more than 20 years. For another material tested (a specific PP liner) the lifetime at same conditions would be less than 6 years. This span shows the importance of careful liner selection. Test reports for testing of different liners in the period 2000 to 2013 can be found in Danish at the Danish Technological Institute [2].

The development of high temperature polymer liners has accelerated as the demand grows. Newly developed high temperature HDPE liners are claimed and guaranteed by the supplier to have a lifetime of more than 20 years at 90°C constant. This liner is used for the SUNSTORE 3 storage in Dronninglund, but it is not tested yet according to the method from the Danish Technological Institute.

The cost of a HDPE liner is app 16 €/m^2 including installation and welding which represents 4 to 5 €/m^2 (budget from SUNSTORE 3).

A new PP liner has been developed with a stated lifetime guarantee of 33 years at 95°C. But with a relatively high the water vapour permeability. Material price similar to the HDPE, but installation price more expensive.

Elastomer liners

EPDM liners have a higher temperature resistance than PP and PE liners, and would be useful above 90°C. EPDM is not weldable and has to be bonded by special vulcanising glue. The price including installation is app. 25% higher than for HDPE liners. Another disadvantage of an EPDM liner is that the vapour permeability is around double as high as for HDPE liners [4]. For the bottom and side liner for a pit heat storage this is not a major problem. If it is used for floating liner in a cover construction the vapour penetration has to be handled in order to avoid moisturizing and decomposition of the insulation used.

Metal liners

Metal liners have the advantage over polymer and elastomer liners that they can resist very high temperatures and they are water vapour tight. The disadvantage is the material cost and the installation cost which are considerably higher.

In a project sponsored by the Danish district heating organisation there has been focused on the development of liners for pit heat storages. The project is carried out by PlanEnergi, Marstal District heating company, The Danish Technological Institute and Force Technology. In this project the material cost for a stainless-steel liner or an aluminium liner was estimated to be app. 3 times as high as for a HDPE liner. In addition to this the installation costs are estimated to be double as high.

For metal liners it is very important to be aware of corrosion issues. On the water side it is possible to secure a water chemistry that is non-harmful to as well grades of stainless steel as grades of aluminium. The water chemistry and steel grade should be evaluated by a corrosion specialist. On the soil side the corrosion behaviour is more unpredictable. In general, stainless steel in an acid proof grade (AISI 316) or Duplex grade is considered suitable, but it has to be evaluated by a corrosion specialist for a specific case.

The metal liners can be delivered in coils of up to 1.500 mm width and welded on site. The most promising welding technique is an induction welding where bending along the edges are welded together by a special induction welder (see figure 5). This process has been used in a 3000 m^3 pit heat storage (Tubberupvænge). The storage was made in 1990 with EPDM lining but due to unacceptable leakage it was covered with a stainless-steel liner in 1997. The welding equipment is today not available as standard equipment and has to be manufactured for the purpose.

Figure 5. Induction welding of a stainless-steel liner [5]

Floating cover

The top surface of the pit heat storage is covered by an insulated floating cover. The cover is the most expensive part of the storage and therefore a lot of effort has been put into investigations of different designs and materials. The overall designs investigated in Denmark can be divided into three categories:

1- Cover based on flexible insulation mats
2- Cover based on Stiff insulation elements
3- Cover based on bulk insulation

The first category is based on flexible insulation mats contained within a watertight floating liner and a top liner. The flexibility allows the insulation to cover the water surface and the edges of the storage as a single unit while the surface is allowed to move up and down due to thermal expansion of the water. Base materials for the insulation are typically polymers or elastomers. For the SUNSTORE 3 and 4 storages a flexible insulation type has been used (Nomalen 28N from NMC). Nomalen is based on a chemically cross-linked polyethylene foam with a closed cell structure. The base material is LDPE, but the cross linking makes the insulation more heat resistant than ordinary LDPE. According to the supplier the material has a working temperature of up to 95°C. The Danish technological institute has evaluated the temperature stability from data from the supplier and expects the Nomalen insulation to be as resistant to high temperatures as the HDPE liners used for floating cover. According to the Danish Technological Institute it is though important to avoid water vapour in contact to the insulation because of the risk of condensing water inside the foam cells.

The second category is based on stiff insulation elements either floating directly on the water or contained between watertight liners as for the flexible cover. Stiff insulation elements made of e.g. PUR or PIR foam typically have better temperature and moisture resistance than flexible insulation made of polymer. When using elements in direct contact to the water special care must be taken because the insulation material itself cannot withstand the hot water over time. Therefore, the insulation material must be coated or contained in a vapour tight lining. Different kinds of polyurea coating has been tested but experiments have shown that this is insufficient. From the experiments it was concluded that a metal lining was necessary, and a 0.75 mm aluminium plate could solve the problem. The thickness and grade of aluminium has to be carefully chosen with respect to water chemistry and corrosion. Because of the low flexibility of the insulation special care has to be taken along the edges of the storages to handle temperature expansion of the insulation elements and changes of water level due to thermal expansion of the water. An almost 20 years old pit heat storage of 1 500 m^3 (Ottrupgaard) has a cover based on stiff insulation elements and is still in operation.

The third category is based on bulk insulation like e.g. expanded clay or expanded glass balls. The insulation is contained between a watertight floating liner and a top liner. Because of the open structure of the insulation and the fact that the temperature is high below the insulation and low above the insulation there is a high risk of significant convection. This has to be investigated for the specific grade of insulation and eventual precautions like convection barriers have to be built into the cover. Also, for the bulk insulation it is important to be aware of the material properties with respect to moisture. When using expanded clay there is a risk that the insulation will absorb moisture and thereby have a significant lower insulation value. Calculations have been carried out to prove that this can be avoided by relatively low ventilation of the insulation, but it is not demonstrated in reality. Because there is limited cohesiveness in the bulk insulation there is also a risk that the insulation particles will not remain in the same place as when installed because of movements of the cover by weather impact, temperature expansion etc. To avoid clumping of the insulation with areas losing the insulation value this has to be considered in the design. To keep the water level as steady as possible it should also be advised to counteract temperature expansion by pumping in and out water from the storage to a reservoir. A cover based on expanded clay insulation will be implemented on pit heat storages in the Danish cities Gram and Vojens in 2015.

Floating lid construction

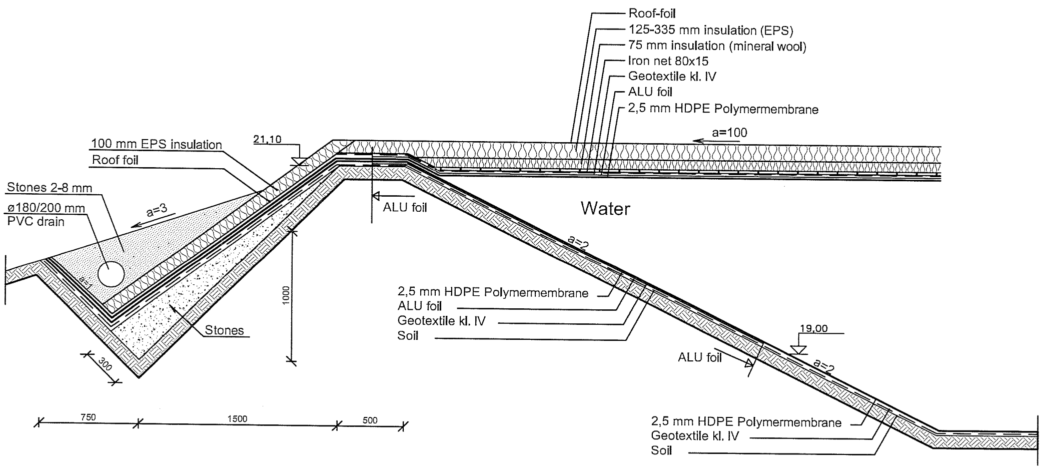

Figure 6. Example of PTES construction (Marstal, DK). Source: PlanEnergi.

The overall requirements for the lid construction- within the lifetime (e.g. 20 years) - are:

a) The liner(s) under the insulation shall be able to withstand the occurring temperatures[2].
b) A liner under the insulation shall be (almost) vapor tight even at the highest temperatures occurring
c) Insulation material shall not absorb humidity (as this will increase heat loss) and humidity shall quickly be vented out of the insulation section
d) Insulation material shall be able to withstand humidity at 90°C
e) The upper liner (above the insulation) shall be raintight
f) Any water inside the lid construction shall drain out
g) Rainwater shall drain from the liner[3]

Conc. a) & b) Temperature resistance and vapour tightness of liner

So far, the best liner solutions found for high temperatures (up to 90°C) are PP and HDPE liners designed for high temperatures. It is important to have a credible lifetime estimate from manufacturer for the specific estimated storage temperature time profile.

Conc. c) Humidity in insulation layer

Some insulation foams are resistant to humidity absorption, e.g. some types of cross-linked polyethylene foam. An example of air venting is shown in the figure below:

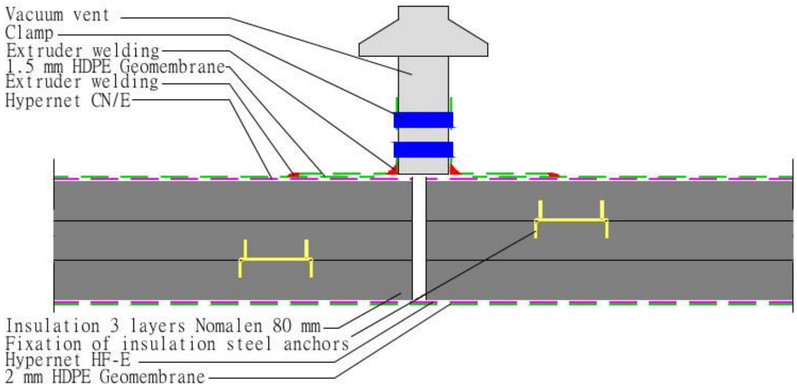

Figure 7. Section view of the cover with air-vent (PlanEnergi).

Conc. d) Rain tightness

Upper liner shall be weatherproof including UV resistant, and shall and tight joints/welds.

Conc. e) & f) Water drainage

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[2] Same requirement for the insulation material, but that is normally not a problem

[3] Could be active pump assisted drainage

Channels in the lid can be made for attracting the water and leading it to central points for pumping to outside the lid. See figures below

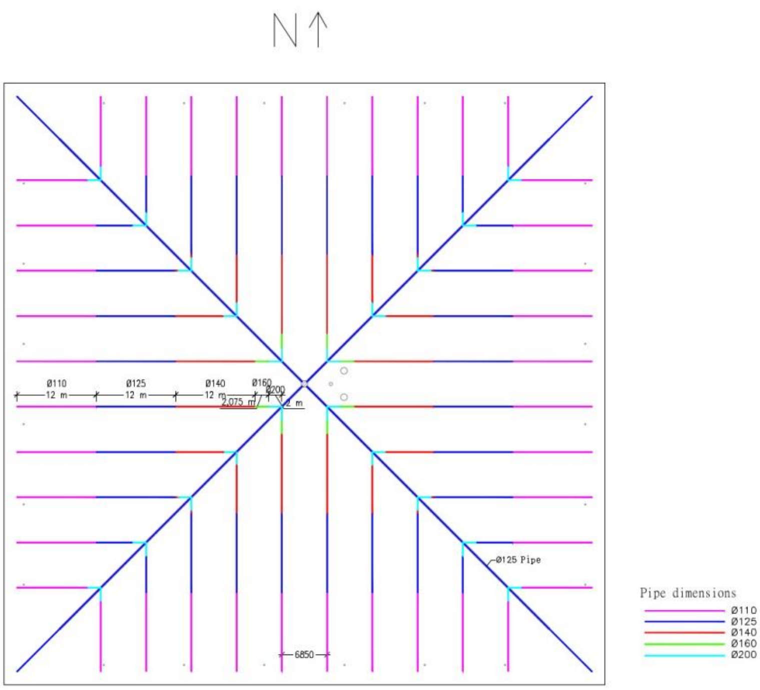

Figure 8. Example of a layout of the weight pipes on the floating liner (PlanEnergi)

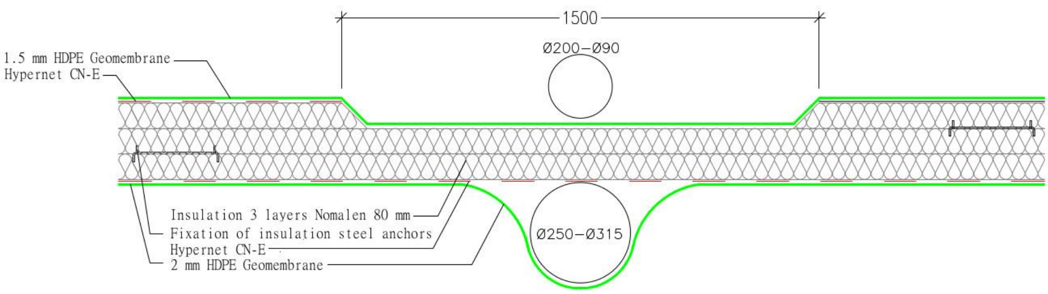

Figure 9. Section drawing of the weight pipe on the floating liner (PlanEnergi)

In-/outlet arrangement

To be able to get energy to and from the storage an in-/outlet arrangement is used. The in-/outlet arrangement consists of at least two pipe connections: One pipe connection led to the bottom of the storage and one pipe connection led to the top of the storage. Dependent on the system connected to the storage and the flexibility wanted it can be advisable with three or five pipe connections in different levels.

The pipe connections can be led through the top cover, the side, or the bottom of the storage. In the SUNSTORE 3 storage it is led through the bottom of the storage and in the SUNSTORE 4 storage it is led through the side of the storage. Pipe connection through the cover has not been implemented in the Danish storages. The pipe connection through the side or bottom liner must be sealed very carefully to avoid leakage. This can be done by welding a flange to the pipes and clamp the liner between the flange and a collar by a bolt connection. A temperature and moisture resistant gasket is placed between the steel flange and the liner. Directly outside the storage the pipes are kept in place by a concrete construction.

The advantage of letting the pipes enter the bottom of the storage is that the pipes enter the storage perpendicular to the liner. This makes the concrete construction below the liner and the flange connection simpler. The disadvantage compared to a pipe connection through the sides is that the pipes must be buried deeper in the ground (below the storage).

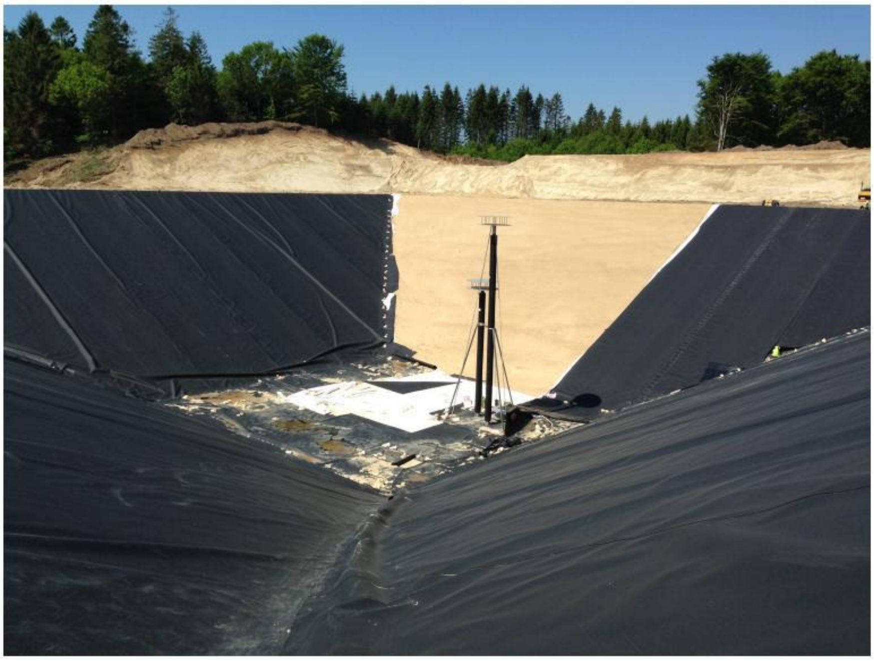

Figure 10. In-/outlet arrangement led through the bottom of the storage. Three pipes ending in a diffusor in the top, the bottom and the volume middle of the storage. Photo from the implementation of the SUNSTORE 3 storage in Dronninglund.

Figure 11. In-/outlet arrangement led through the side of the storage. Photo from the implementation of the SUNSTORE 4 storage in Marstal.

The in/-outlet arrangement can be made of stainless steel or mild steel with or without surface coating. Regardless of the steel type it is important to secure a water chemistry in the storage that will not cause corrosion of the steel parts. Corrosion can happen very fast because of the high temperature of the water. When using stainless steel, the water chemistry is naturally not as critical as when using mild steel but in both cases a corrosion specialist should be consulted to secure a long-lasting combination of materials and water chemistry.

Water quality

Water quality is important because of the steel parts in contact with the storage water. Not only the in/-outlet arrangement but also the piping, heat exchangers, pumps and eventual steel liner. During filling of the storage, the water is softened by a water treatment system and eventually filtered by reverse osmosis. At the same time care should be taken to avoid particles of soil etc. to enter the storage during filling. If severe dirt has entered the storage during filling it can be necessary to clean the storage after the storage is filled and finished with cover. It has been seen that severe contamination of soil particles in the storage can lead to bacterial corrosion of steel parts and clogging of heat exchangers.

After filling of the storage, the water can be treated to avoid corrosion dependent of the steel quality used. Typically, the pH-value is raised to a level around 9,8 to minimize corrosion of steel parts but it depends on the materials used. If aluminium parts are used a pH value of more than 8 will cause corrosion of the aluminium parts.

Location of storage and geotechnical conditions

Ground water conditions

Before establishing the storage some very important initial investigations must be carried out. To avoid excessive heat loss from the storage it is important that the storage is not implemented in an area with floating ground water above the bottom level of the storage. If there is floating groundwater the storage has to be placed above the level of floating ground water. If the ground water is stationary or with negligible flow the storage can in principle be implemented but the ground water level has to be lowered during the implementation phase until the storage is filled with water.

Geotechnical investigations

To determine whether the soil can be used as bottom and sides for the liner and especially whether the excavated soil can be used as embankments around the storage it is necessary with geotechnical investigations. These investigations also help to define how steep it is possible to make the sides of the storage. A steeper storage is an advantage in relation to the size of the cover and thereby the implementation cost and the heat loss of the storage. Typically, the sides of the storage can be made by an inclination of 1 on 2 (26.6° relative to horizontal). During implementation of the storage compression tests of the soil in the embankments should be carried out to ensure the stability of the embankments. The process of the geotechnical investigations is described in [6]

Calculation and optimization of pit heat storages

To be able to predict the behaviour and performance of a pit heat storage in an energy system it is necessary to carry out calculations of the complete system. This can be done by making a mathematical model to simulate the system. The simulation can be done by different tools. The Danish energy systems with seasonal storages have been simulated in the software: TRNSYS.

Simulation tool (TRNSYS)

TRNSYS is a graphically based software for simulating the behaviour of transient systems. It is primarily used for thermal and electrical energy systems. The modelling in TRNSYS is not straightforward and demands knowledge within TRNSYS simulation and the physics of energy systems.

When designing a pit heat storage, it is necessary to know or simulate the system that it interacts in. This could typically be parameters such as the heat consumption from a district heating system, the heat supply from different sources e.g. a solar plant, and meteorological data. The simulation is typically carried out in an hourly basis to simulate how it interacts and behave hour by hour throughout a year.

The pit heat storage can be modelled in TRNSYS with 3 different models, for 3 different types of usages. The simplest one is called the ‘XST model’ (TRNSYS Type 342), developed by TransSolar. This model assumes that the storage has a cylindrical shape with vertical walls (see left part of Figure 12). This model is 2-dimensional as it assumes full rotational symmetry of the storage and the surrounding ground layers, which makes it fast to calculate. This model is used for quick pre-feasibility studies, where parametric studies can be run to achieve system optimization. It is also sufficiently precise to give a good indication of what the yearly storage heat losses will be.

Two other and more sophisticated TRNSYS components for modelling PTES have been developed. One of these is the “truncated cone” component (TRNSYS Type 1300 and 1301), developed by Natural Resources Canada and TESS. This model assumes that the storage has the shape of an inverted truncated cone (see central part of Figure 12). It is divided into two TRNSYS components: one for modelling the storage itself (Type 1300) and one for modelling the surrounding soil (Type 1301). The interactions between the storage and the soil are modelled by connections between these two components. This model (like the XST model) is 2-dimensional, as it assumes full rotational symmetry of the storage and the surrounding ground layers. Though less fast than the XST model, it can be used for feasibility studies, with a more detailed approach. It provides results that are in good accordance with measurements taken from implemented PTES and can therefore be used both for design optimization purposes and performance evaluation (control strategy, heat losses through the top, sides and bottom of the PTES, heat input/output, etc.). It can therefore be used as a reference when comparing a measurement campaign with simulation results.

The other recently developed TRNSYS component for modelling PTES is the “truncated pyramid” component (TRNSYS Type 1322), developed by TESS. This model assumes that the storage has the shape of an inverted truncated pyramid (see right part of Figure 12). This model is 2-dimensional in modelling the storage itself (it models the water as multiple layers of equal volume and temperature) but 3-dimensional in modelling the surrounding ground layers. This model is the most sophisticated PTES model currently available for TRNSYS and fits best to the usual PTES geometry found in Denmark. It does, however, have longer calculation times than the XST model and the truncated cone model, especially when the truncated pyramid model is set to model the storage and soil in detail. This model should be used in the context of a detailed scientific study, provided it can be compared with precise measurement data.

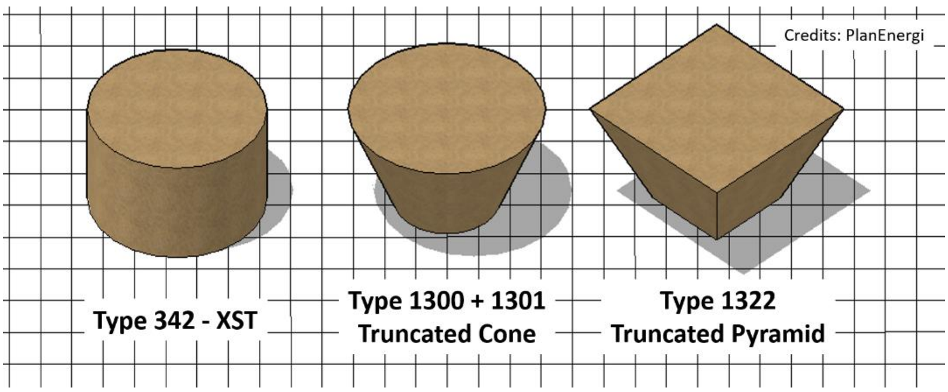

Figure 12. Geometry used for the three PTES components in TRNSYS: Type 342, Type 1300 + Type 1301 and Type 1322

To set up the 3 TRNSYS types, it is also necessary to define parameters as conductivity, heat capacity and fluid density for the storage fluid, as well as thickness and conductivity for the insulation. For the surrounding ground it is also necessary to define conductivity and heat capacity. Direct measurements from the location where the study is being made are thus important requirements for a relevant and realistic feasibility study.

For pit heat storages integrated in an overall system, it is also important to find the correct dimensions of the individual parts of the system.

Figure 13 shows the user interface for a TRNSYS-model that is set up for a Danish CHP plant. The model was used to dimension and optimize the size of a solar plant, a pit heat storage, and an absorption heat pump. From the results it was possible to calculate the profitability of the investment.

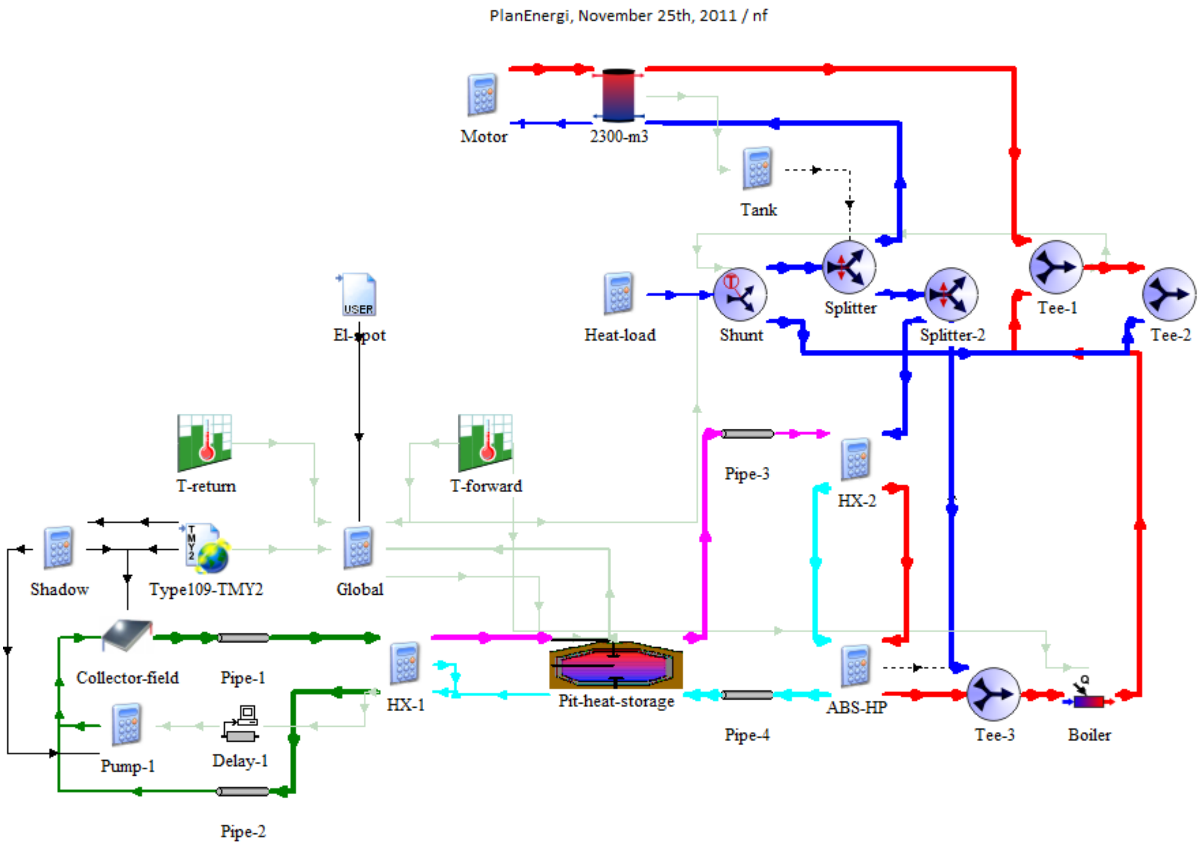

Figure 13. Example of the graphical user interface for a TRNSYS-model of a pit heat storage connected to a district heating CHP plant, a solar collector field, and an absorption heat pump. The model corresponds to the principal diagram of the system shown in figure 14. The model was used to simulate and optimize a system for Gram district heating company.

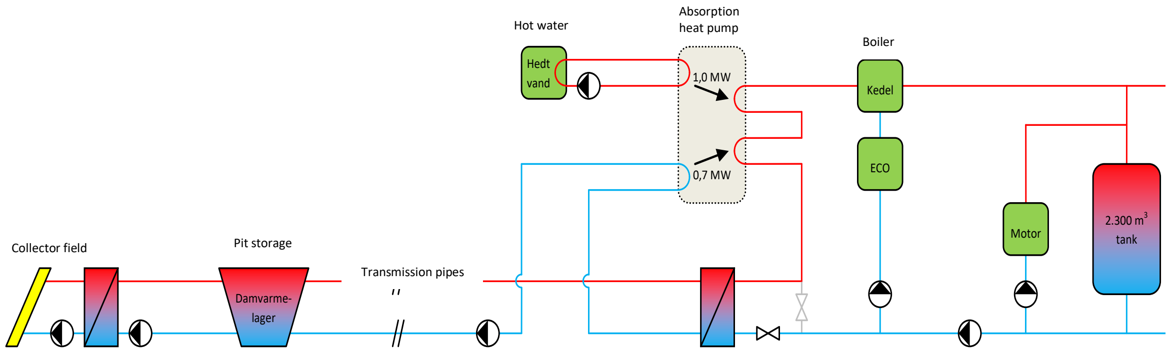

Figure 14. Principal diagram made for Gram District heating company by PlanEnergi. The system consists of a solar plant, a pit heat storage and an absorption heat pump connected to a CHP plant.

Costs of pit heat storages

Based on the experiences from the implemented storages in Denmark the price curve in figure 15 is made. The economy of scale is clear. Going from 60 000 m^3 to 500 000 m^3 the expected specific costs are reduced by more than 20% (from approx. 50 to approx. 30 €/m^3).

But it should be noted that the storage costs are **very much** depending on local conditions and storage/lid construction.

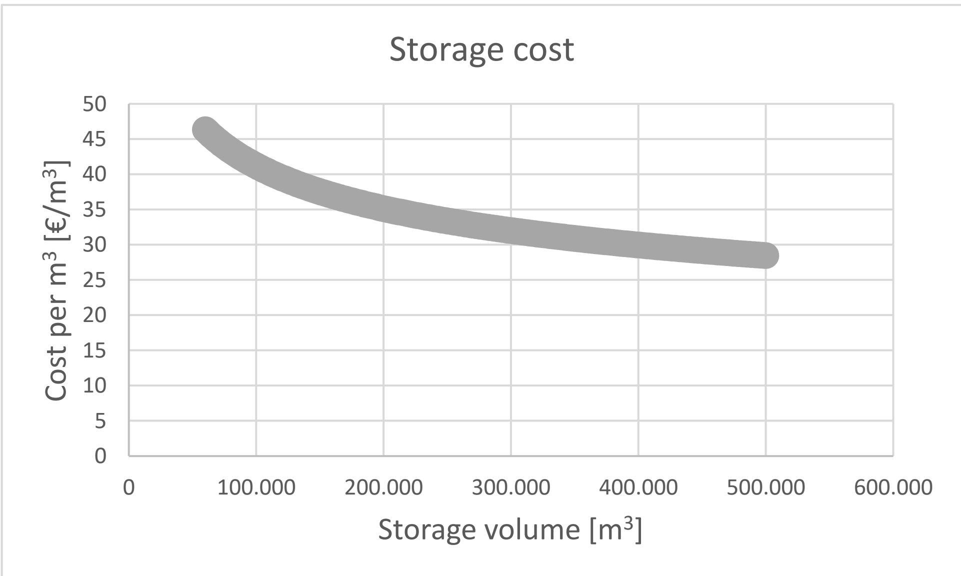

Figure 15. Estimation of the costs for a pit heat storage as a function of the size of the storage. Source: PlanEnergi.

Examples of pit heat storages

In the following three examples of pit heat storages implemented in Denmark are described.

Marstal, SUNSTORE 2

- Built: 2003
- Size: 10,000 m^3
- Price: 0.670 million €, equivalent to 67 € / m^3 or 1.05 € / kWh
- Temperature range: 35-90° C
- Capacity: 638 MWh
- Load and discharge power: 6,510 kW (corresponding to the associated solar installations max. Power).
- Losses: 402 MWh / year (calculated)

Marstal District Heating received in 2001 the grant from the Danish Energy Agency and the EU's 5th framework programme to expand solar collector area of 9,000 m^2 to 18,300 m^2. The solar thermal would then cover about solar 30 % of the annual heat demand. The need for storage of solar heat is at the same time increased, and for that purpose there was included a pit heat storage in the project of 10,000 m^3. The pit heat storage was a further development of the heat storage in Ottrupgård on two essential points.

The clay sealing with EPDM liner on the back side was replaced by a liner made of polyethylene (PE), which could be welded. Before that, three liners were tested at the Danish Technological Institute (a PP liner and two PE liners). The PE-liners showed the longest durability. [2].

The assembly of the lid were changed so that the lid was fixed (in Ottrupgård the lid moves up and down with the water surface) and was constructed on the site. Calculations showed that steam would penetrate the cover bottom liners made of HDPE and condense in the insulation of mineral wool. Therefore, a vapor barrier of 3-layer PE combined with 2 layers of aluminium was admitted.

The structural changes should ensure a price reduction while the durability of the storage was expected to be more than 20 years. The goal was to test a storage construction, which for stores above 50,000 m^3 could be established for less than 35 €/m^3. Figure 6 (page 8) shows a cross-section of the store.

The storage was established during the summer of 2003. During the establishment of the storage some problems with the handling of HDPE liner occurred. The liner is black and was expanding rapidly in the sun, creating big folds that had to be straightened simultaneously with the filling of water.

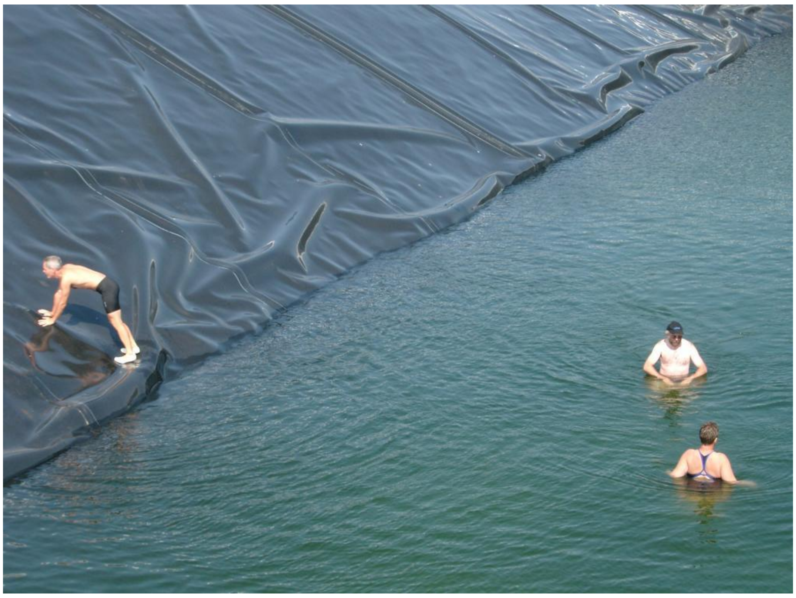

Figure 16 The folds are inspected under the water filling [10].

At the time, the storage was completely filled with water a leak was found at the inlet- and pumping pipes. The leakage was found at a location where there is no channel to be welded (and pressure tested) and was caulked by a diver by means of a HDPE jacket which was filled with silicone.

Figure 17 Inlet and outlet pipes. The leak was in the liner weld during one of the pipes [10].

During operation of the storage the following problems were found:

• There was air (freed from the water by heating) that formed air pockets under the lid. When the lid is not rigid, the pockets grew bigger and bigger.

• There were formed water ponds at the lid terminals. The lid is held down by the valves, which form the vacuum when there is wind, but at the same time are pressing down a little in the lid to form a hollow which can be filled by rain water. When the water does not evaporate before the next rains, this fills additional water in, and the lid is sinking further.

• After 2 years of operation a leak was found in the lid. The leak occurred at the manhole where there was used a corrugated tube of the wrong HDPE material. By this the insulation was filled with water, and both mineral wool and EPS took so much water that the insulating capacity virtually disappeared.

• For subsequent cutting of the lid, it was found that the PE / aluminium vapor barrier was not intact, and the solution will therefore not be implemented in the future.

Marstal, SUNSTORE 4

- Constructed: 2011-12
- Size: 75,000 m^3
- Price: 2.67 Mio. € excl. transmission line, corresponding to 35.7 € / m^3 or 0.375 € / kWh
- Temperature range: 10 - 90 °C
- Capacity: 6,960 MWh
- Load and discharge power; 10.5 MW (equivalent to the coupled collectors)
- Loss (calculated): 2,475 MWh / year

Marstal District Heating received in 2010 grants from the EU's 7th framework programme for the expansion of energy production plant, for the solar thermal to cover up to half of the heat demand, and the rest of the heating requirement to be covered by wood chips from a wood-fired cogeneration plant. The solar heating system was increased by 15,000 m^2 to 33,300 m^2 and there was added 75,000 m^3 pit heat storage, a heat pump of 1.5 MW_{heat}, a wood chip boiler of 4 MW and an Organic Rankine Cycle of 750 kW.

A principal diagram is shown in figure 18.

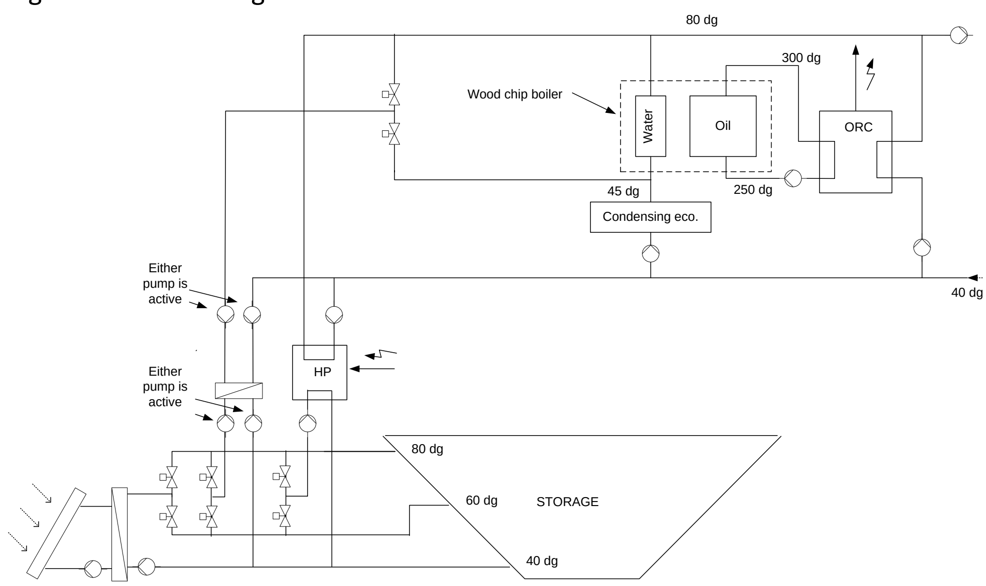

Figure 18 Principal diagram of the SUNSTORE 4 project [11].

The pit heat storage was a development of the 10,000 m^3 storage, established under the SUNSTORE 2 project. The below points should be amended:

- Formation of air pockets under the lid was to be prevented.
- Formation of water ponds on top of the lid should be prevented.
- The insulation should be water-resistant.
- The vapor barrier should be changed.

The principle of the assembly of the lid is to use drill collars to get the lid to fall toward the centre so that rainwater is collected and pumped away from a pump sump. The lid is moving with the water surface. The inventory design was like in the SUNSTORE 2 project (truncated cone sealed with plastic liner and inclination 1:2). The lid solution is shown in figure 19.

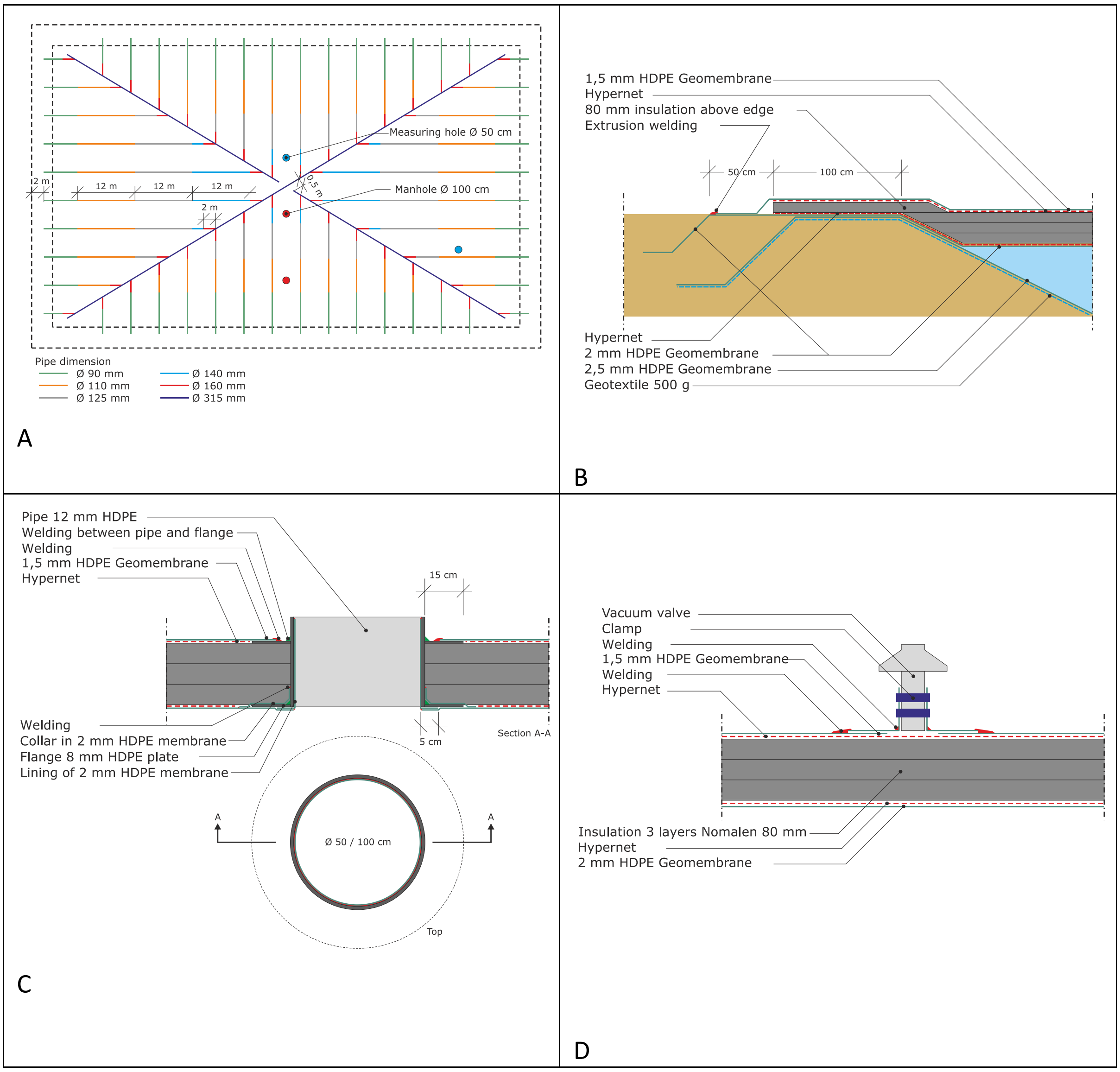

Figure 19 Drawings of the lid solution in the SUNSTORE 4 project [12]. A: top view of the lid with the drill collar shown. B: edge solution. C: manhole. D: cuts with vacuum valve.

The storage should have been established during the summer and autumn of 2011, but a cloudburst in mid-August slowed the work so much that the side and bottom liners had to be established in November. The water filling took place in December 2011 and January and February 2012. The work with the lid construction took place from April 2012 and the storage was heated from July 2012.

Especially excavation to the storage caused major problems due to a rainy summer. Fitting the side and bottom liner went smoothly because of the very lucky weather in November. Fitting the lid was difficult because there could not get any water into the lid.

Figure 20 Construction of the storage in Marstal [13]. a: inlet and outlet pipes are hoisted into place. b: the storage after the cloudburst. c: The liner work. d: the lid is built.

Dronninglund, SUNSTORE 3

- Constructed: 2013
- Size: 60,000 m^3
- Price: approx. 2.28 Mio. € excl. transmission lines corresponding to 37.9 € / m^3 or 0.416 € / kWh
- Temperature range: 10 - 90°C
- Capacity: 5,570 MWh
- Input and pumping capacity: 26.1 MW (equivalent to solar panels max. Output power)
- Loss (calculated): 2,260 MWh / year

Dronninglund District Heating was in 2009 granted EUDP support for an energy production system consisting of 35,000 m^2 of solar panels, 60,000 m^3 pit heat storage and a 3 MW heat pump. The construction phase is first initiated in the spring of 2013, partly due to that the storage had to be moved, partly because of neighbour objections to the plan authorization. The excavation into the heat storage is made from mid-March to mid-May 2013 and the liner work was completed in mid-June, where after the water filling began. The construction is as in Marstal, but the following precautions are taken to prevent corrosion:

- The water is cleaned from limestone and salts (osmosis)
- pH is kept at 9.8
- Water quality is monitored regularly during and after filling
- The storage is cleaned from dirt before the water filling
- A diver cleans from dirt when the lid closes the storage
- Filters are placed before heat exchangers, to prevent clogging

Inlet and outlet arrangement are made of stainless steel.

Figure 10 (page 11) shows a picture of the storage under construction.

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